# A Proposal for Amendment to the City of Lawrence Building Code Concerning Basement Wall Insulation

Neal Ezell April, 2008

### Background

The city of Lawrence has adopted the 2006 International Residential Code (IRC) which prescribes the minimum use of either R-13 cavity insulation or R-10 continuous insulation on basement walls to a depth of ten feet or over the entire wall. While this requirement is of vital importance to the overall energy efficiency of structures, it ignores the many practical difficulties faced by compliance. The motivation for this proposed amendment is the concern over how builders will choose to conform to this requirement in unfinished areas.

The methods builders are likely to use and the difficulties that will be faced by each are outlined below.

## Method 1 – Stud Wall with Batt Insulation

The most obvious method of conformance is to simply construct a stud wall with R-13 batt insulation that is left exposed and unsecured.

The issues with exposed batt insulation are:

- True R-Value In order for batt insulation to yield its rated Rvalue it should be installed in an <u>enclosed cavity</u>.
- Fire Hazard The Kraft backing on batt insulation is not firerated for exposure. Unfaced batts must then be used which have only friction to hold them

in place over the life of the

structure.



Figure 1 – Unfaced fiberglass batts

3) Human Exposure – Research has suggested that fiberglass is a carcinogen. OSHA requires that bags of fiberglass insulation carry a cancer warning label.

The insulated stud wall could be covered with drywall to alleviate the problems above. However, this would greatly increase costs and require partial removal and destruction for future renovations which is costly and wasteful.

### Method 2 – Exterior Foam Board

An alternative method is to use high-density polystyrene on the exterior of walls to full depth. This method involves many of the same obstacles as slab insulation, which precipitated an amendment to allow its exclusion. These obstacles include: termite shield, protection against damage, brick ledge issues and porch or patio connections.

### Method 3 – Interior Foam Board

Another alternative is to use interior foam board insulation. According to International Building Code (IBC) 2603.4, foam plastic insulation must be separated from the interior with  $\frac{1}{2}$ " drywall. Two inch thick polystyrene foams are rated R-10 and cost about \$0.69/square foot, while 1-1/2" polyisocyanurate (polyiso) is R-9 and costs \$0.60/square foot. However, polyiso has a low permeability that makes it a poor candidate for use on sub-grade concrete (see attachment A). This is because sub-grade concrete cannot dry to the exterior. Even small amounts of moisture from cracks or small imperfections in the damp-proofing can cause serious implications if it is not allowed to dry to the interior.

### **Proposed Methods**

Polyiso foam board (see attachment B) can be installed to a depth of 3 feet below grade on the interior of concrete walls, which allows the wall to dry to the inside through the bottom of the wall. The foam board along with its drywall covering can be secured to the wall with Tapcons<sup>TM</sup> or an equivalent fastener through 1-1/2'' washers.

This method has the following benefits:

- 1) It is easy to install and remove in case of future renovations
- 2) Low cost (\$ 3.60 per lineal foot)
- 3) Nearly the same performance as the code prescribes
- 4) Greatly reduced moisture issues
- 5) Secure, safe and durable



Figure 2 – R-9 polyiso foam board

A similar alternative is to build a stud wall and insulate with R-13 batts to a depth of 3 feet below grade, which could then be covered with drywall. This method would allow most future wiring to be easily installed without major destruction.

Neither of these proposed methods currently conforms to code because of the depth requirement. However, the following analysis will show that this compromise has little effect on a home's energy efficiency.

To demonstrate the effectiveness of the proposed methods, a simulation was run on a test home. The test home (attachment C) is a simplified two story with a full-in basement. It has 1008 square feet on each of three levels (28'x36') with half of the basement level finished. Using the REScheck software two different scenarios were simulated to compare them to the absence of insulation. In each scenario the attic was insulated with R-38, walls in finished areas with R-13, Low-E windows were used (10% of above grade finished space), and standard fiberglass front and rear doors. REScheck determined the maximum UA for the structure to be 356.

### Uninsulated

Walls in the unfinished parts of the basement were left uninsulated resulting in a UA of 411.

## Proposed Method (R-9 on Top Four Feet)

Walls in the unfinished parts of the basement were insulated with R-9 continuous insulation on the top four feet resulting in a UA of 341. Note that R-9 continuous and R-13 cavity insulation provides nearly identical results.

## Code Prescribed Method (R-10 on Entire Wall)

Walls in the unfinished parts of the basement were insulated from top to bottom with R-10 continuous insulation resulting in a UA of 328.

Using no insulation does not meet the minimum UA requirement, though the addition of a 92 AFUE furnace does cause compliance. The proposed method yields an overall envelope improvement of 17%, while the code prescribed method results in a further improvement of just 4% while more than doubling the cost.

This analysis demonstrates the relative importance of insulating the top of the wall where the top is exposed to ambient air and the remainder lies above the

frost line. The relative stability of soil temperatures three or more feet below grade acts as an energy sink. This prevents energy conduction through the concrete wall. Intuitively, insulating the wall ten feet below grade makes little sense unless one is also prepared to insulate under the basement floor as well where the soil is nearly the same temperature. The R-value of 9 was used since this is readily available in 1-1/2" thick polyisocyanurate.

It turns out that the difference between four feet of R-9 and eight feet of R-10 is 0.2 UA per lineal foot, independent of the configuration of the structure. The difference between eight feet of R-10 and no insulation is 1.3 UA per lineal foot. Therefore, according to REScheck, the top four feet accounts for 85% of basement wall UA contribution versus 15% for the lower half.

It must be pointed out that the above analysis is restricted to UA, which is not the same as an analysis of energy savings, especially in our mixed climate. In contrast to above grade walls, subgrade wall insulation applied below 3' is only an advantage in winter months. Though the ambient temperature in summer may be 100 degrees, the soil temperature below three feet will range from 55-60 degrees—a distinct advantage in summer.

To determine the relative impact these scenarios have on actual energy savings, the test home was simulated using REM/Design software. This software is used by most Home Energy Rating System (HERS) inspectors. Attachments D and E show the results of comparisons of the above methods in dollars with the cost of the improvements amortized at a rate of 6% for a cash flow analysis.

		H	eating &		Net	(	Cost of	(	Cash	C	ost per
Method	UA	Co	oling Cost	Sa	vings	Imp	rovements	I	Flow	Lir	eal foot
Uninsulated	411	\$	1,120	l	N/A		N/A		N/A	\$	0
Proposed	341	\$	992	\$	128	\$	331	\$	104	\$	5.17
Code Prescribed	328	\$	968	\$	151	\$	671	\$	103	\$	10.48

Table 1 – 2-Story simulation results

Table 1 shows a summary of the results of these software simulations. The comparison of no insulation with the proposed method in attachment D yields a reduction in total heating and cooling costs of 11%. Attachment E compares no insulation with the code prescribed method to yield a reduction in heating and cooling costs of 14%. Also note that both measures show a small monetary loss for cooling costs as expected. Though the code prescribed method offers a 4% improvement in UA, it yields only a 3% savings in direct energy costs over the proposed method. When the extra costs of the improvements are considered, the cash flow is reduced.

### **Rancher Analysis**

Another interesting analysis was performed by deleting the 2<sup>nd</sup> floor from the test home and leaving the basement entirely unfinished. This simulation represents the opposite extreme configuration. The results are listed in Table 2.

		He	eating &		Net Cost of		Cost of Cash		C	ost per	
Method	UA	Coc	oling Cost	Sa	vings	Improvements F		mprovements Flow		Lir	ieal foot
Uninsulated	377	\$	917	I	N/A	N/A			N/A	\$	0
Proposed	237	\$	662	\$	256	\$	662	\$	208	\$	5.17
Code Prescribed	212	\$	614	\$	303	\$	1,341	\$	206	\$	10.48

Table 2 – Rancher sim	ulation results
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These results again show a reduced cash flow for the code prescribed method relative to the proposed method. The proposed method yields a reduction in total heating and cooling costs of 28%, while the code prescribed method achieves a reduction of 33%. Though the code prescribed method offers a 5% greater savings in energy, its additional cost results in \$2 negative yearly cash flow.

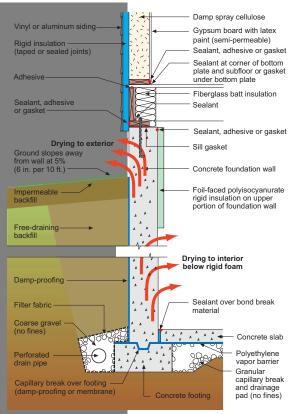
### Conclusion

The addition of basement wall insulation is one of the most cost effective measures to improve energy efficiency in new homes. It can result in energy savings ranging from 10-30% depending on the configuration of the structure. Its use should be encouraged by providing a safe and practical means for its inclusion rather than simply stating a minimum R-value.

This proposal has pointed out that attempting to comply with the code as written can lead to unintended, deleterious effects to building safety. It has also shown that subgrade insulation installed below 3 feet yields only a marginal improvement in overall energy efficiency that cannot be justified by the added monthly costs to the consumer. Therefore, the methods proposed herein should be adopted as an alternative that builders may choose to provide to their customers even if they are not using the prescribed code method.

### List of Attachments

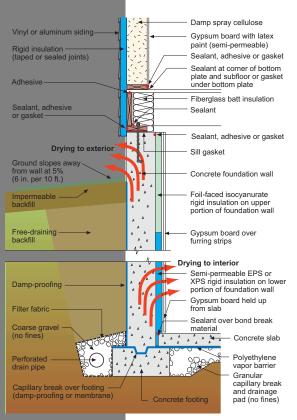
- A) Building Science Corporation study, <u>Basement Insulation Systems</u>, Pg. 12. The remainder of the report is available at: www.eere.energy.gov/buildings/building\_america/pdfs/db/35017.pdf
- B) Atlas Roofing Corporation, AC Foam  $II^{TM}$  product specifications.
- C) Test home floor plan.
- D) REM/Design improvement analysis of R-9 polyiso on top four feet of wall.
- E) REM/Design improvement analysis of R-10 polyiso on entire wall.



#### Figure 11

Unfinished basement with half-height insulation

- Lower portion of wall dries to the interior
- Upper portion of wall dries to the exterior



#### Figure 12

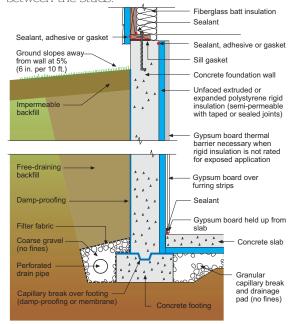
Finishing basement at a later date

- Drying continues to the interior
- Drying to the exterior

The fastest and most cost effective way to provide insulation is covering the upper half of the foundation wall with foil-faced polyisocyanurate foam sheathing that is fire rated for exposed use (**Figure 11**). This will eliminate the greatest source of heat transfer through the foundation wall while still allowing the lower half of the wall to dry to the interior. The joints between pieces of foam sheathing must sealed using foil tape to prevent air leakage that could result in condensation on the cold foundation wall.

If at a later date the wall is to be finished, expanded polystyrene (EPS) can be used to cover the lower half of the wall (**Figure 12**). Expanded polystyrene is semi-permeable to water vapor and will allow the lower portion of the wall to continue to dry inwards. However, the expanded polystyrene will require thermal protection with 0.5 inch of gypsum board or equivalent.

Keeping the gypsum board off the floor a minimum of 0.5 inch will prevent wetting of the gypsum board in the event of small leak or flood. If a frame wall is placed interior to the rigid insulation, cavity insulation without a vapor barrier or retarder can be installed between the studs.



### Figure 13

Full height basement insulation

· Upper and lower portion of wall can dry to interior



from damage by construction traffic and/or

abuse is extremely important. Roof surface

protection such as plywood must be used

in areas where storage and staging are

FM Standard 4450/4470 Approval

http://www.atlasroofing.com/commercial/acfoam2.asp

ACFoam-II is approved for Class 1 insulated steel, wood, concrete and gypsum roof deck construction for 1-60 and 1-90 Windstorm Classifications (may

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be mopped or mechanically fastened to concrete roof decks). Refer to FM Approval Guide for details on specific systems.

#### **UL Standard 1256 Classification**

Insulated metal deck construction assemblies - Construction #120 and #123.

#### UL Standard 790 (ASTM E 108) Classification

Class A with most roof membrane systems. See UL Roofing Materials & Systems Directory.

#### UL Standard 263 Fire Resistance Classification (ASTM E 119)

Some classifications for fire resistance are P225, P230, P259, P508, P510, P514, P519, P701, P710, P713, P717, P718, P719, P720, P722, P723, P724, P725, P727, P728, P729, P730, P732, P801, P814, P815, P818, P819, and P828. See UL Fire Resistance Directory for updated listings.

**UL Standard 1897 Uplift Resistance** 120 psf, 150 psf, 165 psf, 245 psf.

#### UL Certified for Canada

UL of Canada Insulated Roof Deck Assemblies -Construction #C34. CAN/ULC-S126-M86, CAN/ULC-S101-M89, CAN/ULC-S107-M87



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planned and heavy or repeated traffic is anticipated during or after installation. (See Technical Bulletin #00-01)

#### Moisture/Vapor Control

Vapor retarders are used to impede the passage of water vapor into roofing systems, thereby preventing condensation and resulting damage to the insulation and roof system. All Atlas Roof Insulation Products may be installed with or without a vapor retarder, the need for which is determined by the designer. The designer may consult the NRCA Roofing and Waterproofing Manual for guidance in determining the need for a vapor retarder. Special consideration should be given to construction-generated moisture, as well. For example, construction-generated moisture, such as will be released by placing concrete floor slabs after the roof has been installed, can drive large quantities of moisture into the roof system. Therefore, Atlas cannot be responsible for damage to the insulation when exposed to construction-generated moisture. Refer to the NRCA Roofing and Waterproofing Manual for their recommendations for the use of a vapor retarder when construction-generated moisture is present (4th Edition, Volume 1, p. 121). Refer to Atlas Technical Bulletin #00-01.



WARRANTY

In response to valid concerns of building designers regarding thermal efficiency of roof assemblies and the long-term insulating value of roof insulation, Atlas offers a 20-year, limited thermal warranty. The "ACFoam" Limited Warranty places Atlas ACFoam products above all others and supports the building owner, designer and contractor by backing up thermal performance. This warranty is available to the building owner at the time the building is completed and is transferable to any subsequent owner for the duration of the 20-year period.

#### Limitation of Liability

Other than the aforementioned representations and descriptions, Atlas Roofing Corporation (hereafter, "Seller") makes no other representations or warranties as to the insulation sold herein. The Seller disclaims all other warranties, express or implied, including the warranty of merchantability and the warranty of fitness for a particular purpose. Seller does, however, have a limited warranty as to the R-Value of the insulation, the terms of which are available upon request from the Seller.

The Seller shall not be liable for any incidental or consequential damages including the cost of installation, removal,

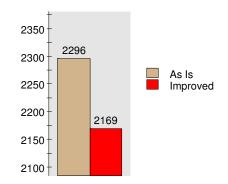
28'-0"			281-0"	
MAIN LEVEL 1008 SF.	36 - 0 =	T-N-504 ST-70	UNFINISHED 504 SF. BASEMENT	
		14'-0"	4 ' - 0 "	
ZND FLOOR 1008 SF.	36'-0"			
		NSTRUCTION, INC.	TEGT 2-STORY SCALE: 1/6" - 1' REVISION DATE: FEORDARY, 2008	1

Building Name:		Date:	April 24, 2008
Owner's Name:		Builder's Name:	
Property		Weather Site:	Topeka, KS
Address:	,	File Name:	Code Amendment.blg

#### Energy Costs (\$/yr)

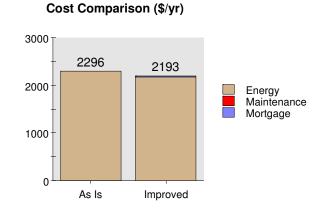
			]
End-Use	As Is	With All Improvements	Savings
Heating	963	833	130
Cooling	157	159	-2
Hot Water	228	228	0
Lights and Appliances	659	659	0
Photovoltaics	-0	-0	0
Service Charge	292	292	0
TOTAL	2299	2171	128

### Total Costs (\$/yr)



#### Information For Lenders and Appraisers

Installed Cost of Improvements (\$)	331
Cost Weighted Life of Measure (Years)	30
Mortgage Term (Years)	30
Discount/Mortgage Rate (%)	6.000
Present Value Factor	13.8
Expected Annual Energy Savings (\$)	128
Expected Annual Maintenance Costs (\$)	0
Expected Annual Savings (\$)	128
Increased Annual Mortgage Costs (\$)	24
Present Value of Savings (\$)	1756
Expected Annual Cash Flow (\$)	104



#### REM/Design - Residential Energy Analysis Software v12.41

Code Amendment.blg						Page 2	
Recommended Improvements							
Measure Costs	Life	Cost	Yr Savings	SIR	PV	SP	
1: Add R-9 polyiso. 4 ft	30	331	128	5.3	1425	2.59	
Criteria							
Ranking Criteria: SIR	Maximum \$ Limit: No Limit						
Cutoff: 0	Measures: Interactive						

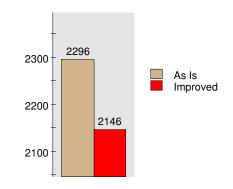
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Building Name:		Date:	April 24, 2008
Owner's Name:		Builder's Name:	
Property		Weather Site:	Topeka, KS
Address:	,	File Name:	Code Amendment.blg

#### Energy Costs (\$/yr)

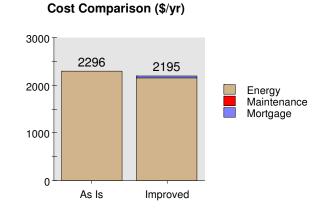
End-Use	As Is	With All Improvements	Savings
Heating	963	809	154
Cooling	157	159	-2
Hot Water	228	228	0
Lights and Appliances	659	659	0
Photovoltaics	-0	-0	0
Service Charge	292	292	0
TOTAL	2299	2148	151

### Total Costs (\$/yr)



#### Information For Lenders and Appraisers

Installed Cost of Improvements (\$)	671
Cost Weighted Life of Measure (Years)	30
Mortgage Term (Years)	30
Discount/Mortgage Rate (%)	6.000
Present Value Factor	13.8
Expected Annual Energy Savings (\$)	151
Expected Annual Maintenance Costs (\$)	0
Expected Annual Savings (\$)	151
Increased Annual Mortgage Costs (\$)	49
Present Value of Savings (\$)	2083
Expected Annual Cash Flow (\$)	103



#### REM/Design - Residential Energy Analysis Software v12.41

Code Amendment.blg					F	age 2
Recommended Improvements						
Measure Costs	Life	Cost	Yr Savings	SIR	PV	SP
1: Add R-10 polyiso. full	30	671	151	3.1	1412	4.43
Criteria						
Ranking Criteria: SIR	Maximum \$ Li	Maximum \$ Limit: No Limit				
Cutoff: 0	Measures: Inte	eractive				

REM/Design - Residential Energy Analysis Software v12.41